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PLASMA FORMATION DURING HIGH PRESSURE LASER WELDING

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INTRODUCTION

Laser welding is one of many processes used at the Los Alamos Scientific Laboratory (LASL) to fabricate prototype assemblies to be used for DOE sponsored programs. The primary application of laser welding at LASL is for assembly of heat sensitive components and/or welding in gaseous environments at pressures significantly above atmospheric. Solid state, pulsed mode Nd-YAG systems are favored to obtain the maximum coupling efficiency, with the wide range of metal alloys used. A characteristic of laser processing is the ability to deliver discrete, precisely defined quantities of energy to the work piece and to perform real time monitoring of the average power (watts) and the pulse characteristic (pulse length) of the laser beam. It has been our experience, that when these operational parameters are controlled and the coupling action of the laser to the substrate in question is well characterized, then the process is sufficiently reliable to produce consistent, repeatable welding results. An exception to this observation is the welding of components in pressurized work chambers. Extremely erratic and unpredictable welding behavior has been experienced when the welding is performed at pressures above atmospheric.

An example of a high pressure welding application is the laser seal welding of inertial fusion (IF) experimental target assemblies. The laser is used to perform a seal weld at pressure and thus produce a gas-filled sealed IF target. This is an extremely sensitive welding procedure and we have encountered difficulties in obtaining consistent welding results, particularly as the gas pressure is increased above ~7 MPa. Investigation of this problem indicates that significant quantities of the laser energy can be absorbed by a plasma plume which is present during the time that the laser beam is interacting with the surface of the target material. Such phenomena have been observed with CO₂, lasers operating at atmospheric pressure and have been well documented in the literature (1,2). However, previous reports dealing with the Nd-YAG system indicate that absorption of laser energy in the plasma is of little importance since a transmission of the Nd-YAG beam is unaffected by the plasma due to the shorter (1.06 μ versus 10.6 μ for CO₂) wavelength of the Nd-YAG and b) the pulsed mode operation of the Nd-YAG where the plasma frequency is sufficiently low to not easily to cause significant laser interaction, do not find no prior reference dealing with laser processing in high pressure environments. A series of tests was performed to attempt to gain a more comprehensive understanding of the problem.

EXPERIMENTAL METHODS

High speed photographic techniques were used to study the plasma formation and its effect on the welding conditions, i.e., at atmospheric pressure in the absence of gas shield gas. The characteristics of the plasma were highlighted by back lighting of the workpiece with a He-Ne laser which was located a few centimeters behind the laser beam incident on the target directly onto the workpiece. In addition, the features were noted for the plasma plume. In addition, the characteristics of the plasma as a function of the pulse length (1.06 μ) pulse shape, pulse repetition

rate (10-200 cps), focus and average power (watts). A flat stainless steel substrate was used as the target material for most of these experiments. Figure 1 shows some selected frames representative of a 7-ms pulse. The plasma plume is fully developed almost instantaneously and the major portion of the laser pulse is, therefore, transmitted through the plume. Figure 2 shows the characteristics of the plume in more detail. An inner intense glow is surrounded by a less brilliant outer fringe which contains substantial quantities of particulates including solid pieces of weld spatter. The plume is extinguished between pulses and appears to conform exactly to the duration of the laser pulse. There was no single parameter that, by itself, had any significant effect on the characteristics of the plume formation. The intensity of the plasma appeared to increase with increased intensity of the laser energy delivered to the work surface.

A second series of experiments was performed using a transparent vacuum box to visually observe the effect of vacuum, argon, and helium gas environments. The laser was directed through a glass window and focused on a stainless steel plate. Figures 3, 4, and 5 show the variation in the visible plume at the various conditions. With a slight positive pressure in argon, the plasma is intense and localized above the target surface. The intensity is significantly less in the helium atmosphere, and in a vacuum of ~10 Torr there is very little plasma effect and the outline of the laser beam is defined, presumably due to the incandescent glow caused by interaction of the laser beam with vaporized metal. The weld penetrations obtained during these tests were also of interest, e.g., the welds in helium were three times as deep as those made in argon and the vacuum welds were twice again as penetrating as the helium welds. It should be noted that, in vacuum, the silicon inner surface is rapidly coated with vapor oxides which results in transmission problems. The final testing was an attempt to measure the effect of high pressure on weld penetration over the pressure range from atmosphere to 70 MPa. Figure 6 shows a schematic of the pressure vessel used for this study. A single pulse from the laser was directed through the sapphire window and focused at the target surface. A series of spot welds were made at varying pressures in hydrogen (deuterium) gas and the penetration measured as a function of gas pressure. Results are shown in Figure 7.

DISCUSSION

When the Nd-YAG laser is used in a welding mode, the interaction of the focused laser beam with the workpiece surface results in the initiation of a plasma plume. The appearance of the plasma corresponds, primarily with the laser pulse width, irrespective of the pulse shape, output frequency, the intensity of the laser beam with the target material, the frequency of the laser radiation, and the type and nature of the penetration.

It is not within the scope of this paper to speculate on the mechanism for initiation of the plasma, however, potential candidates to gas breakdown due to 10, laser interaction with atomic nuclei and Nd-YAG, provide an excellent model to account for this phenomenon given the operating conditions of the Nd-YAG system.

The target of this investigation was the transmission of the laser pulse through a plasma. In the presence of a plasma, added attenuation would be vary inversely with the intensity of the laser and the depth of penetration (depth of tissue melted) is related to the atten-

The results obtained by penetrations at very high pressure are somewhat inconclusive. At this time, we could expect the threshold for the penetration to decrease with increasing pressure with an increase in plasma intensity and laser absorption. The lack of conclusive data relates to problems of conducting this type of experiment, and the relevant data are being reexamined to verify the data. There is, however, some degree of confidence in the general shape of the curve of Figure 7. A possible explanation for the shape of the curve is provided as follows: at low pressures, transmission of the laser radiation is effected with correspondingly good weld penetrations as the pressure and plasma intensity increase, the penetration decreases to a minimum value at which point heat transfer by radiation from the intense plasma becomes a factor in determining the depth of the melt zone. Radiation from the plasma is, therefore, a primary source of surface melting at the highest pressures examined in this investigation.

SUMMARY AND CONCLUSIONS

The plasma plume formed during welding with a pulsed Nd-YAG laser attenuates the laser radiation and directly affects weld penetration. The attenuation is proportional to the intensity of the plasma and, therefore, increases with increase in the gas pressure of the working environment. As the intensity of the plasma increases, heat radiation from the plasma becomes a significant factor contributing to the size of the melt zone.

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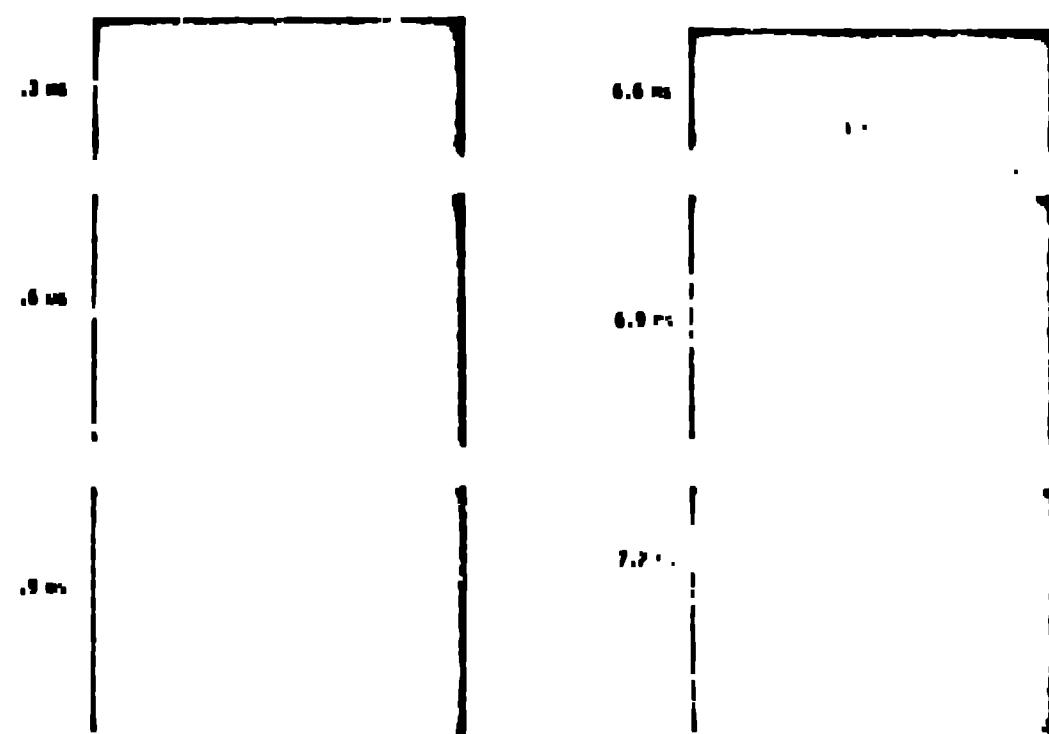


Figure 1. Selected cross sections of welds (100% of the laser energy).



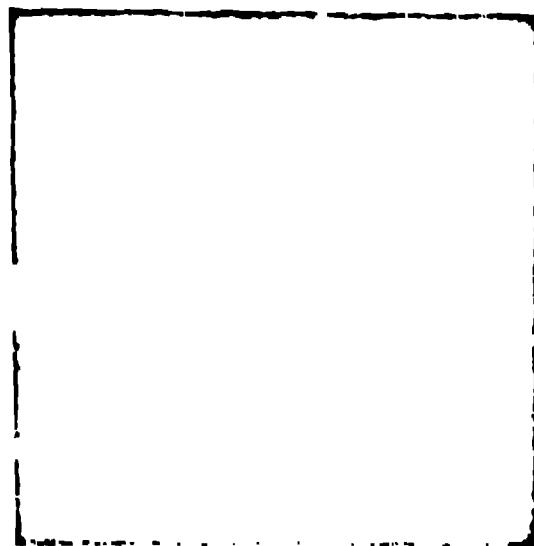
Single frame from 100 f.p.s. motion picture; laser power-350 watts, 7-ms pulse length, 30 ps, focused on stainless steel target material argon gas flow at atmosphere pressure.



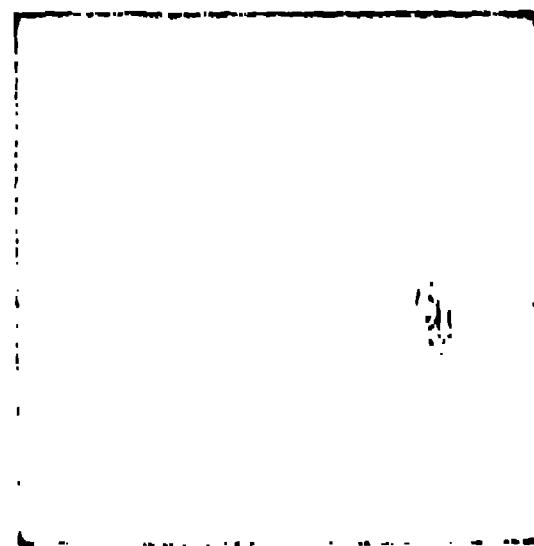
Chamber has slight positive pressure of argon 200 watts average power, 3.2ms pulse length, 30 ps, focused on flat stainless steel plate.

Figure 2 Detail of fully developed plasma plume.

Figure 3 Plasma appearance - welding in argon atmosphere.



As per Figure 2 but with flat plate target material.



As per Figure 4 except vacuum chamber. The plasma plume is brighter and more concentrated than in Figure 4 due to lack of gas.

Figure 4 Plasma appearance - welding on flat plate.

Figure 5 Plasma appearance - welding in vacuum.

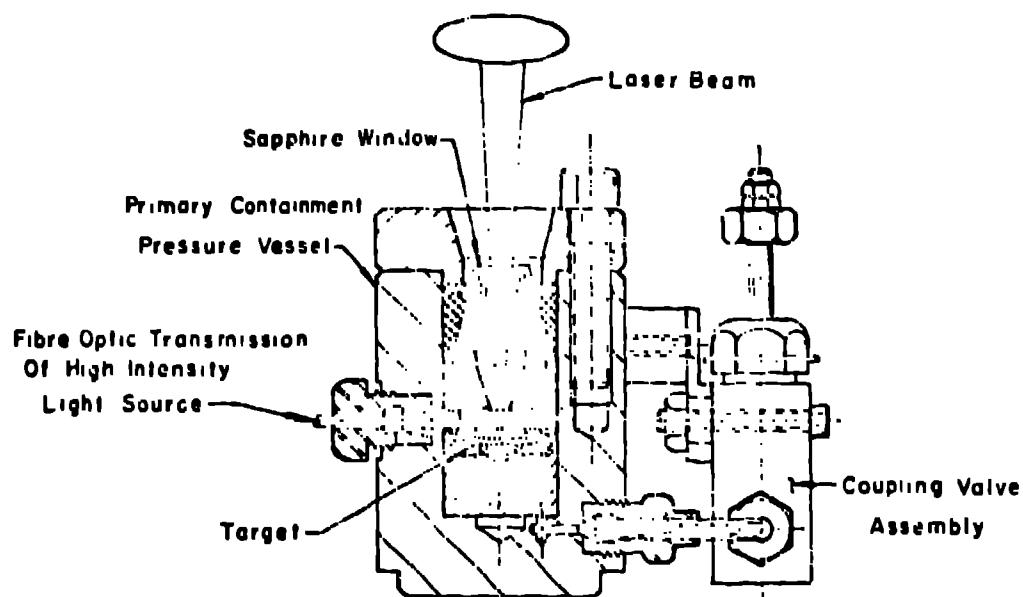


Figure 6 Schematic of pressure vessel used for testing at pressures < 70 MPa.

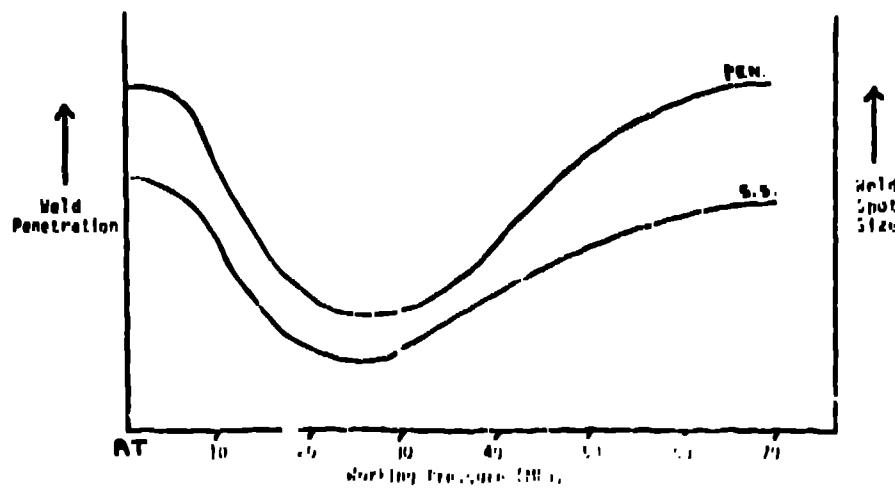


Figure 7 Graphic representation of effect of pressure on weld penetration and weld size.